

2.14

bcc

$$\delta_0 = (0, 0, 0) \cdot a$$

$$\delta_1 = \left(\frac{1}{2}, \frac{1}{2}, \frac{1}{2}\right) \cdot a$$

$$F = \sum_j f_{a_j} e^{i\vec{s} \cdot \vec{\delta}_j} = f_a \left[ 1 + e^{i(h\vec{a}^* + k\vec{b}^* + l\vec{c}^*) \cdot \delta_1} \right]$$

$$= f_a \left[ 1 + e^{i\pi(h+k+l)} \right]$$

$$\Rightarrow \text{when } h+k+l = \text{odd} \quad F = 0$$

$\Rightarrow (100), (111), (210)$  will be missing

fcc

$$\delta_0 = (0, 0, 0) a$$

$$\delta_1 = \left(\frac{1}{2}, \frac{1}{2}, 0\right) a$$

$$\delta_2 = \left(0, \frac{1}{2}, \frac{1}{2}\right) a$$

$$\delta_3 = \left(\frac{1}{2}, 0, \frac{1}{2}\right) a$$

$$\Rightarrow F = 1 + e^{i\pi(h+k)} + e^{i\pi(k+l)} + e^{i\pi(h+l)}$$

$$\Rightarrow F \neq 0 \text{ if } h, k, l \text{ are all even or all odd}$$

$\Rightarrow (100), (110), (210), (211)$  are missing

2.16

$$f_{Cs} = 3f_{Cl}$$

$Cs$  in the corner,  $Cl$  in the center.

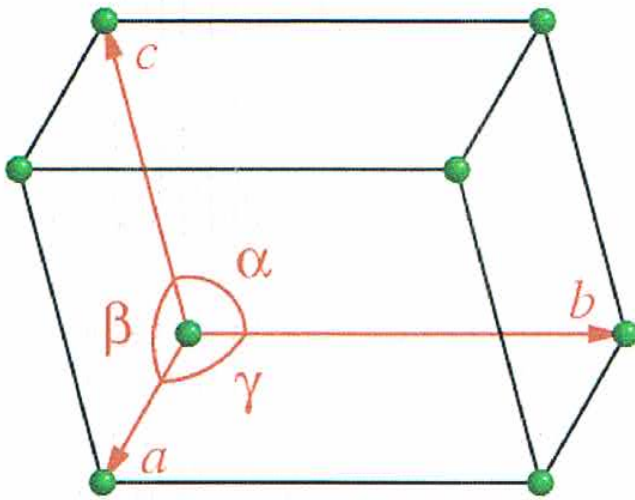
$$\begin{aligned} F_{100} &= f_{Cs} + f_{Cl} e^{2\pi i (\frac{1}{2}h + \frac{1}{2}k + \frac{1}{2}e)} = \\ &= f_{Cl} (3 + e^{i\pi(h+k+e)}) = 2f_{Cl} \end{aligned}$$

$Cl$  in the corner,  $Cs$  in the center

$$F_{100} = f_{Cl} + 3f_{Cs} e^{i\pi(h+k+e)} = -2f_{Cl}$$

In both cases, we notice that  $f_{Cs} \neq f_{Cl}$ , so the lattice can no longer be regarded as the bcc lattice with all the same atoms in the unit cell.

2.20



$$\begin{aligned} a &= 4 \text{ \AA} \\ b &= 6 \text{ \AA} \\ c &= 8 \text{ \AA} \\ \alpha &= \beta = 90^\circ \\ \gamma &= 120^\circ \end{aligned}$$

a)  $\vec{a} = a(1, 0, 0)$

$$\vec{b} = b(\cos 120^\circ, \sin 120^\circ, 0) = b\left(-\frac{1}{2}, \frac{\sqrt{3}}{2}, 0\right)$$

$$\vec{c} = c(0, 0, 1)$$

$$V_c = |\vec{a} \cdot (\vec{b} \times \vec{c})| = |\vec{b} \cdot (\vec{c} \times \vec{a})| = abc \frac{\sqrt{3}}{2}$$

$$\vec{a}^* = \frac{2\pi}{(\frac{\sqrt{3}}{2})abc} \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ -\frac{1}{2} & \frac{\sqrt{3}}{2} & 0 \\ 0 & 0 & 1 \end{vmatrix} = \frac{4\pi}{\sqrt{3}a} \frac{\sqrt{3}}{2} \hat{x} + \frac{4\pi}{\sqrt{3}a} \frac{1}{2} \hat{y} = \frac{2\pi}{a} \hat{x} + \frac{2\pi}{\sqrt{3}a} \hat{y}$$

$$\vec{b}^* = \frac{2\pi}{(\frac{\sqrt{3}}{2})abc} \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ 1 & 0 & 0 \\ 0 & 0 & 1 \end{vmatrix} = \frac{4\pi}{\sqrt{3}b} \hat{y} = \frac{2\pi}{3\sqrt{3}} \hat{y}$$

$$\vec{c}^* = \frac{2\pi}{(\frac{\sqrt{3}}{2})abc} \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ 1 & 0 & 0 \\ -\frac{1}{2} & \frac{\sqrt{3}}{2} & 0 \end{vmatrix} = \frac{4\pi}{\sqrt{3}c} \frac{\sqrt{3}}{2} \hat{z} = \frac{2\pi}{c} \hat{z} = \frac{\pi}{4} \hat{z}$$

b) Volume of the real cell:

$$V_c = abc \frac{\sqrt{3}}{2} = 4 \cdot 6 \cdot 8 \cdot \frac{\sqrt{3}}{2} = 166.24 \text{ \AA}^3$$

Volume of the reciprocal cell

$$\frac{(2\pi)^3}{V_c} = \frac{(2\pi)^3 \cdot 2}{abc \sqrt{3}} = 1.49 \text{ \AA}^{-3}$$

c) The spacing between the (210) planes

$$d_{210} = \frac{1}{\left(\frac{2^2}{4^2} + \frac{1}{6^2}\right)^{\frac{1}{2}}} = 1.89 \text{ \AA}$$

d) The Bragg angle  $\theta$  for reflection from the above planes.

$$2d_{210} \sin \theta = \lambda$$

$$\Rightarrow \theta = \sin^{-1}\left(\frac{\lambda}{2d_{210}}\right)$$

2.21

$$\gamma = \frac{dV}{V}$$

$$2d \sin \theta = \lambda$$

$$\frac{d}{d\theta} (2d \sin \theta) = \frac{d\lambda}{d\theta}$$

$$d \cos \theta + \sin \theta \frac{d(d)}{d\theta} = 0$$

$$d\theta = -\tan \theta \frac{d(d)}{d}$$

$$V = c d^3 \quad \leftarrow \text{some constant}$$

$$V dV = 3d^2 d(d) \Rightarrow \frac{d(d)}{d} = \frac{dV}{3d^3} = \frac{dV}{3V} = \frac{\gamma}{3}$$

$$\Rightarrow d\theta = -\frac{\gamma}{3} \tan \theta$$

3.2 Since both longitudinal (compressional) and transverse (shear) waves can be transmitted by the solid, and since their speeds are different, we replace  $v_s$  in (3.20) by

$$\frac{3}{v_s^3} = \left( \frac{1}{v_e^3} + \frac{2}{v_t^3} \right)$$

$$\Rightarrow g(\omega) = \frac{V}{2\pi^2} \omega^2 \left( \frac{1}{v_e^3} + \frac{2}{v_t^3} \right)$$

3.4

$$Z = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \exp\left(-\frac{1}{k_B T} \left[ \frac{p^2}{2m} + \frac{1}{2} k x^2 \right]\right) dp dx =$$

$$= \int_{-\infty}^{\infty} \exp\left(-\frac{p^2}{2mk_B T}\right) dp \int_{-\infty}^{\infty} \exp\left(-x^2 \left(\frac{k}{k_B T}\right)\right) dx =$$

$$k = m\omega^2 \quad \beta = \frac{1}{k_B T}$$

$$= \sqrt{2mk_B T \pi} \sqrt{\pi k_B T / m\omega^2} = \pi k_B T / \omega = \frac{\pi \hbar}{\beta \omega}$$

$$E = -\frac{\partial}{\partial \beta} \ln Z = \frac{1}{\beta} = k_B T$$



3.8

$$E = \frac{3V}{2\pi^2 v_s^3} \int_0^{\omega_D} \frac{\hbar \omega^3}{e^{\hbar\omega/k_B T} - 1} d\omega$$

$$C_V = \left( \frac{dE}{dT} \right)_V = \frac{3V}{2\pi^2 v_s^3} \int_0^{\omega_D} \frac{\hbar \omega^3 \frac{\hbar \omega}{k_B} \frac{1}{T^2} e^{\hbar\omega/k_B T}}{(e^{\hbar\omega/k_B T} - 1)^2} d\omega$$

$$= \frac{3V \hbar^2}{2\pi^2 v_s^3 k_B T^2} \int_0^{\omega_D} \frac{\omega^4 e^{\hbar\omega/k_B T}}{(e^{\hbar\omega/k_B T} - 1)^2} d\omega$$

$$x = \frac{\hbar\omega}{k_B T} \quad \theta_D = \frac{\hbar\omega_D}{k} \quad \Rightarrow \quad \omega = \frac{x k_B T}{\hbar}$$

$$C_V = \frac{3V \hbar^2 (k_B T)^5}{2\pi^2 v_s^3 k_B T^2 \hbar^5} \int_0^{\theta_D/T} \frac{x^4 e^x dx}{(e^x - 1)^2} =$$

$$= \frac{3V k_B^4 T^3}{2\pi^2 v_s^3 \hbar^3} \int_0^{\theta_D/T} \frac{x^4 e^x dx}{(e^x - 1)^2}$$

$$\omega_D = v_s (6\pi^2 n)^{1/3} = v_s \left( 6\pi^2 \frac{N_A}{V} \right)^{1/3}$$

$$\Rightarrow v_s^3 = \left( \frac{\theta_D k_B}{\hbar} \right)^3 \frac{V}{N_A 6\pi^2}$$

$$\Rightarrow C_V = \frac{3V \hbar^2 k_B^4 T^3 N_A 6\pi^2 \hbar^3}{2\pi^2 V \theta_D^3 k_B^3 \hbar^3} \int_0^{\theta_D/T} \frac{x^4 e^x dx}{(e^x - 1)^2} =$$

$$= 9R \left( \frac{T}{\theta_D} \right)^3 \int_0^{\theta_D/T} \frac{x^4 e^x dx}{(e^x - 1)^2} dx$$